



Robust Actuator Fault Diagnosis for LPV systems: Application to Quadrotor

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> Prepared by: Eslam Abouselima

Under supervision of: Prof. Said Mammar Prof. Dalil Ichalal



Presentation outlines





Problem statement

Proposed solution

Solution synthesis





Proposed solution

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Results



FTC importance for automated systemsWhy quadrotor?







FDD scheme







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 $\begin{cases} \dot{x}(t) = A(\rho(t)) x(t) + B(\rho(t)) u(t) + F(\rho(t)) f(t) + E(\rho(t)) d(t) \\ y(t) = C(\rho(t)) x(t) + D(\rho(t)) u(t) \end{cases}$

where

LPV model:

$$M(\rho(t)) = \sum_{k=1}^{w} \mu_k(\rho(t)) M_k,$$

w:no.of vertices



Why LPV modeling?





u(*t*) =
$$-K(\rho(t)) \hat{x}(t) + V(\rho(t)) \eta(t)$$

Lyapunov inequality:

 $(A_k - B_k K_k)^T P + P(A_k - B_k K_k) + 2\zeta_c P \le 0$

Proposed solution

Robust H_{∞} control

Bounded real lemma:

$$\begin{pmatrix} (A_k - B_k K_k)^T P + P(A_k - B_k K_k) & P B_k & C_k^T \\ B_k^T P & -\gamma_c I & D_k^T \\ C_k & D_k & -I \end{pmatrix}$$

DC gain

Control law:

$$V_k = -(C_k (A_k - B_k K_k)^{-1} B_k)^{-1}$$





Proposed solution



Observer scheme:

$$\begin{cases} \dot{\hat{x}}(t) = A_{\rho} \, \hat{x}(t) + B_{\rho} \, u(t) + L_{\rho}(y(t) - \hat{y}(t)) \\ \hat{y}(t) = C_{\rho} \hat{x}(t) + D_{\rho} u(t) \\ r(t) = y(t) - \hat{y}(t) \end{cases}$$

The system:

$$\begin{aligned} \dot{x}(t) &= A_{\rho} x(t) + B_{\rho} u(t) + F_{\rho} f(t) + E_{\rho} d(t) \\ y(t) &= C_{\rho} x(t) + D_{\rho} u(t) + J_{\rho} f(t) + H_{\rho} d(t) \end{aligned}$$

Resulting error dynamics:

$$\begin{cases} \dot{e}(t) = (A_{\rho} - L_{\rho} C_{\rho})e(t) + (F_{\rho} - L_{\rho} J_{\rho})f(t) + (E_{\rho} - L_{\rho} H_{\rho})d(t) \\ r(t) = C_{\rho}e(t) + J_{\rho}f(t) + H_{\rho}d(t) \end{cases}$$



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Proposed solution

The new approach

The system:

Differentiated output: $\tilde{y}(t)$

$$\dot{x}(t) = A_{\rho}x(t) + B_{\rho}u(t) + F_{\rho}f(t) + E_{\rho}d(t)$$

$$y(t) = C_{\rho}x(t) + D_{\rho}u(t)$$

$$\tilde{y}(t) = \frac{d}{dt}$$

$$y(t)$$

System classification according to the relative degree $\lambda_f > \lambda_d$ $\lambda_f < \lambda_d$ $\tilde{y}(t) = C_{\overline{\rho}} x(t) + B_{\overline{\rho}} u(t) + R_{\overline{\rho}} f(t) + D_{\overline{\rho}} \bar{d}(t)$ $\tilde{y}(t) = C_{\overline{\rho}} x(t) + B_{\overline{\rho}} u(t) + R_{\overline{\rho}} f(t)$ $\lambda_f = \lambda_d$ $\tilde{y}(t) = C_{\overline{\rho}} x(t) + B_{\overline{\rho}} u(t) + R_{\overline{\rho}} f(t) + D_{\overline{\rho}} d(t)$

$$\tilde{y}(t)$$
 $\frac{d}{dt}$ $y(t)$

Proposed solution

The new approach

The proposed residual generator:

$$\begin{cases} \dot{\hat{x}}(t) = A_{\rho}(t) \, \hat{x}(t) + B_{\rho} \, u(t) + L_{1\overline{\rho}} \big(y(t) - \hat{y}(t) \big) + L_{2\overline{\rho}} \big(\tilde{y}(t) - \hat{\tilde{y}}(t) \big) \\ \hat{y}(t) = C_{\rho} \hat{x}(t) \\ \hat{\tilde{y}}(t) = C_{\overline{\rho}} \, \hat{x}(t) + B_{\overline{\rho}} \, u(t) \\ r(t) = M_{\overline{\rho}} \big(\tilde{y}(t) - \hat{\tilde{y}}(t) \big) \end{cases}$$

Reference residual signal:

$$r_r(t) = Q f(t)$$

Virtual residual signal:

$$r_e(t) = r(t) - r_r(t)$$



Proposed solution



The new approach

Post bandpass filter

$$\begin{cases} \dot{x}_h(t) = A_h x_h(t) + B_h r_e(t) \\ r_f(t) = C_h x_h(t) + D_h r_e(t) \end{cases}$$







Proposed solution

Solution synthesis

Results

Solution synthesis



□ Applying for system of case 2 ($\lambda_f = \lambda_d$)

Error dynamics become $\dot{e}(t) = (A_{\rho} - L_{1\overline{\rho}}C_{\rho} - L_{2\overline{\rho}}C_{\overline{\rho}}) e(t) + (E_{\rho} - L_{2\overline{\rho}}D_{\overline{\rho}}) d(t) + (F_{\rho} - L_{2\overline{\rho}}R_{\overline{\rho}}) f(t)$ $r_{e}(t) = M_{\overline{\rho}} C_{\overline{\rho}} e(t) + M_{\overline{\rho}}D_{\overline{\rho}} d(t) + (M_{\overline{\rho}}R_{\overline{\rho}} - Q)f(t)$

Theorem (1): Exact residual convergence

 $r_r(t) = Q f(t) \rightarrow r_{e(t)} = 0$

Condition to satisfy: rank $\begin{pmatrix} \begin{bmatrix} C_{\overline{\rho}} & R_{\overline{\rho}} & D_{\overline{\rho}} \\ 0 & Q & 0 \end{bmatrix} = rank (\begin{bmatrix} C_{\overline{\rho}} & R_{\overline{\rho}} & D_{\overline{\rho}} \end{bmatrix})$ The gains $M_{\overline{\rho}} = \begin{pmatrix} 0 & Q & 0 \end{pmatrix} (C_{\overline{\rho}} & R_{\overline{\rho}} & D_{\overline{\rho}})^{-1}$, $L_{1\overline{\rho}}$, $L_{2\overline{\rho}}$ can be chosen freely

Solution synthesis



□ Applying for system of case 2 ($\lambda_f = \lambda_d$)

Error dynamics become

$$\dot{e}(t) = (A_{\rho} - L_{1\overline{\rho}}C_{\rho} - L_{2\overline{\rho}}C_{\overline{\rho}}) e(t) + (E_{\rho} - L_{2\overline{\rho}}D_{\overline{\rho}}) d(t) + (F_{\rho} - L_{2\overline{\rho}}R_{\overline{\rho}}) f(t)$$

 $r_e(t) = M_{\overline{\rho}} C_{\overline{\rho}} e(t) + M_{\overline{\rho}} D_{\overline{\rho}} d(t) + (M_{\overline{\rho}} R_{\overline{\rho}} - Q) f(t)$

Theorem (2): Asymptotic residual convergence

$$\begin{cases} \lim_{t \to \infty} r(t) = Q f, & d = 0 \\ \|r(t) - Q f(t)\|_{2} \le \gamma \|d(t)\|_{2}, & d \neq 0 \end{cases}$$

Condition to satisfy: $rank(R_{\overline{\rho}}) = n_{f}, \quad rank\left(\begin{bmatrix}F_{\rho}\\R_{\overline{\rho}}\end{bmatrix}\right) = rank(F_{\rho})$
The gains $M_{\overline{\rho}} = QR_{\overline{\rho}}^{-1}, \ L_{2\overline{\rho}} = F_{\rho} R_{\overline{\rho}}^{-1}, \ L_{1\overline{\rho}}$ is chosen to minimize disturbance effect.

Solution synthesis



□ Applying for system of case 2 ($\lambda_f = \lambda_d$)

Error dynamics become $\dot{e}(t) = (A_{\rho} - L_{1\overline{\rho}}C_{\rho} - L_{2\overline{\rho}}C_{\overline{\rho}}) e(t) + (E_{\rho} - L_{2\overline{\rho}}D_{\overline{\rho}}) d(t) + (F_{\rho} - L_{2\overline{\rho}}R_{\overline{\rho}}) f(t)$ $r_{e}(t) = M_{\overline{\rho}}C_{\overline{\rho}} e(t) + M_{\overline{\rho}}D_{\overline{\rho}} d(t) + (M_{\overline{\rho}}R_{\overline{\rho}} - Q)f(t)$

Worst case H_{-}/H_{∞} technique

The gains $M_{\overline{\rho}}$, $L_{2\overline{\rho}}$, $L_{1\overline{\rho}}$ *are chosen to minimize disturbance effect and maximize fault effect such that:*

 $\left| \left| T_{rd} \right| \right|_{\infty} \le \gamma$ $\left| \left| T_{rf} \right| \right|_{\infty} \ge \beta$





Proposed solution

Solution synthesis

Results



\Box Reference tracking using H_{∞} control





□ Residual generator in fault free case





\Box New approach vs H_{-}/H_{∞} technique





□ Battery level estimation





Post bandpass filter importance







Proposed solution

Solution synthesis

Results





□ LPV modeling gives more realistic and dynamic system model.

□ Robustness of the controller is very essential feature.

 \Box The H_{-}/H_{∞} observer is enhanced greatly using the auxiliary output.

□ Some structural properties of the system may simplify fault estimation.

□ A post bandpass filter can improve the obtained residual signal.





□ Fault compensation in case of partial loss of actuators efficiency.

□ Controller reconfiguration in case of one or more actuators failure.

□ Applying the developed algorithms in real time on a drone.



THANK YOU



Questions?